# The use of thermal analysis in the study of Ca<sub>3</sub>Al<sub>2</sub>O<sub>6</sub> formation by the polymeric precursor method

I. Lazău · C. Păcurariu · R. Băbuță

ESTAC2010 Conference Special Issue © Akadémiai Kiadó, Budapest, Hungary 2011

**Abstract** Single-phase Ca<sub>3</sub>Al<sub>2</sub>O<sub>6</sub> was prepared via polymeric precursor method. The influence of the reactants nature in the Ca<sub>3</sub>Al<sub>2</sub>O<sub>6</sub> synthesis was investigated. For this purpose, citric acid and soluble salts of calcium (nitrate, chloride, carbonate) and aluminium (nitrate, chloride, acetate) were used as starting materials, in the presence and, respectively, in the absence of ethylene glycol. Ca<sub>3</sub>Al<sub>2</sub>O<sub>6</sub> resulted as single-phase after annealing at 1050 °C for 1 h only starting from calcium nitrate or carbonate and aluminium nitrate or acetate as salts precursor for Ca<sup>2+</sup> and Al<sup>3+</sup> cations. The formation of Ca<sub>3</sub>Al<sub>2</sub>O<sub>6</sub> is not conditioned by the ethylene glycol presence in these mixtures. Using calcium and aluminium chlorides, the phases present at 1050 °C are Ca<sub>12</sub>Al<sub>14</sub>O<sub>33</sub> and unreacted CaO.

**Keywords** Calcium aluminates · Pechini method · Polymeric precursor method · Thermal analysis

### Introduction

Tricalcium aluminate,  $Ca_3Al_2O_6$  or  $3CaO \cdot Al_2O_3$  ( $C_3A$ ) is one of the important mineralogical compounds in the Portland cement composition. Beside the wide use of  $C_3A$ in the cement technology, recently has been reported the possibility to produce a novel red light-emitting material  $Ca_3Al_2O_6:Eu^{3+}$ , in which the activator  $Eu^{3+}$  is hosted in the lattice of  $Ca_3Al_2O_6$  [1]. Tricalcium aluminate has also been successfully used as doping phase for improving the

I. Lazău · C. Păcurariu (⊠) · R. Băbuță

Faculty of Industrial Chemistry and Environmental Engineering, "Politehnica" University of Timişoara, P-ta Victoriei No. 2, 300006 Timişoara, Romania

r-ja victoriei No. 2, 500000 rimişoara, Komama

e-mail: cornelia.pacurariu@chim.upt.ro

bioactivity and biocompatibility of the calcium aluminate bone cement [2] and nickel support as catalyst for methane partial oxidation to syngas (CO and  $H_2$ ) [3].

The preparation of  $C_3A$  via conventional methods based on annealing mechanical mixtures of oxides, hydroxides and/or salts, requires high temperatures (1200–1400 °C) and is always preceded by the formation of various intermediate phases such as  $Ca_{12}Al_{14}O_{33}$  ( $C_{12}A_7$ ) or  $CaAl_2O_4$ (CA) [4–6].

To avoid the disadvantages of the conventional route, many chemical unconventional methods have been developed for the  $C_3A$  synthesis [7–29].

Stephan and Wilhelm [7] used the sol-gel method for the C<sub>3</sub>A synthesis. Only after three annealing cycles of 14 h at 1260 °C with intermediate grindings they obtained C<sub>3</sub>A together with insignificant amounts of CaO and C<sub>12</sub>A<sub>7</sub>.

Douy and Gervais [8] prepared pure  $C_3A$  at 1230 °C using spray-drying of calcium and aluminium nitrates aqueous solution.

The use of some complex combinations as precursors for preparing  $C_3A$  has been also attempted [9, 10]. Using as precursor the complex combination resulted by oxidation of ethylene glycol by calcium and aluminium nitrates, Lazău et al. [9] prepared  $C_3A$  as single-phase at 1000 °C.

A solution-polymerization route, based on polyvinyl alcohol as polymer carrier [11-13] represents another alternative for preparing C<sub>3</sub>A.

The combustion method was also investigated for the calcium aluminate synthesis [14–19]. Taş reported [16] the synthesis of pure C<sub>3</sub>A after annealing the powders at 1050 °C for 48–72 h using urea, carbohydrazide or glycine as fuel. The use of fuel mixtures in the combustion method represents a significant innovation noticed by Ianoş et al. [17–19]. This new approach allows obtaining pure C<sub>3</sub>A,

directly from the combustion reaction, without any further annealing, using a mixture of urea and  $\beta$ -alanine as fuel [19].

In the past years, Pechini method (also known as the citrate route or polymeric precursor method) has been widely reported for the synthesis of many oxide powders [20–24].

Invented by Pechini [25], this process involves a polyester-type resin formation which represents the polymeric carrier for the pre-ceramic powder. In this route, citric acid acts as a chelating agent of the dissolved metal cations. The cation sources are soluble salts, usually nitrates. By heating the solution of these chelates and a polyhydroxy alcohol (usually ethylene glycol) at temperatures between 150 and 250 °C, the polycondensation reaction takes place and results in the resin formation, in which the metal cations are uniformly distributed.

This method was also investigated for the synthesis of different calcium aluminates [26–29]. Using nitrates salts and a molar ratio citric acid/total cations = 1, Gaki et al. [26] obtained pure  $C_3A$  after annealing at 1000 °C for 3 h. Starting from aluminium nitrate and calcium carbonate, Yuan et al. [29] studied the influence of the molar ratio citric acid/total cations on the  $C_3A$  formation. For molar ratio citric acid/total cations = 1, respectively, 2, the annealing temperature for obtaining  $C_3A$  was 1100 °C for 2 h, whilst when using a molar ratio citric acid/total cations = 4, single-phase  $C_3A$  was obtained after annealing at 1000 °C for 2 h.

The article deals with a systematic and original study regarding the influence of the reactants nature in the  $C_3A$  synthesis using the polymeric precursor's method.

The behaviour of the polymeric precursor depending on the thermal treatment conditions has been also investigated.

#### Experimental

The raw materials used were:  $Ca(NO_3)_2 \cdot 4H_2O$  (Reactivul, Romania),  $CaCl_2 \cdot 2H_2O$  (Reactivul, Romania),  $CaCO_3$ (Reactivul, Romania),  $Al(NO_3)_3 \cdot 9H_2O$  (Merck, Germany),  $AlCl_3 \cdot 6H_2O$  (Reactivul, Romania),  $Al(OH)(CH_3COO)_2$ (Riedel de Haën, Germany), citric acid (Chimopar, Romania) and ethylene glycol (Reactivul, Romania). The compositions of the studied samples are presented in Table 1.

The difference between the samples 1, 3 and 4 was the nature of the salts used as the source for the  $Ca^{2+}$  and  $Al^{3+}$  cations, in order to emphasize the role that they play in obtaining  $C_3A$  as single-phase. The molar ratio  $Ca^{2+}/Al^{3+}$  for all the four samples was the same, 3/2, in order to result  $C_3A$ .

Starting from the literature data [29], the citric acid was taken in excess over the stoichiometric amount needed. We worked with the molar ratio citric acid/Ca<sup>2+</sup>/Al<sup>3+</sup> = 15/3/2. The molar ratio citric acid/ethylene glycol was established in

order to ensure the esterification of all –COOH groups by the citric acid excessively used.

The polymeric precursor for the four samples was prepared by the following procedure: the calcium and aluminium salts, in the molar ratios presented in Table 1, were dissolved in the aqueous solution of citric acid at the temperature of 60–70 °C, resulting in a homogeneous solution. Ethylene glycol was added (sample 2 excepted) to the obtained solution under continuous heating.

After complete water evaporation, the reaction mass undergoes a polycondensation process. The resulted resin represents the precursor for the  $C_3A$  formation after thermal treatments at temperatures between 600 and 1050 °C.

Investigations regarding the mechanism of  $C_3A$  synthesis were performed via thermal analysis using a NET-ZSCH-STA 449C instrument. The TG/DTA curves were recorded in the range 25–1200 °C with a heating rate of 10 K min<sup>-1</sup>, using platinum crucibles. The experiments were carried out in nitrogen atmosphere and also in artificial air at a flow rate of 20 mL min<sup>-1</sup>. Samples were also characterized by means of IR spectroscopy. FTIR spectra were carried out using a Shimadzu Prestige-21 spectrometer in the range 400–4000 cm<sup>-1</sup>, using KBr pellets and resolution of 4 cm<sup>-1</sup>.

The phase composition evolution of the samples was monitored by XRD using a DRON 3 diffractometer with  $Cu_{K\alpha}$  radiation. BET surface area measurements were performed using a Micromeritics ASAP 2020 instrument and nitrogen as adsorption gas.

# **Results and discussion**

The mixture of raw materials corresponding to sample 1 (solution) was subjected to thermal analysis in nitrogen atmosphere (Fig. 1).

The strong endothermic effect at 146.4 °C accompanied by large mass loss on TG curve can be assigned to the removal of the free water and crystallization water. The second endothermic effect at 223.0 °C accompanied also by mass los was assigned to the removal of the water resulted from the polycondensation processes. A small endothermic effect follows on DTA curve, accompanied by mass loss at 400 °C, associated with some degradation processes of the precursor resin. Between 400 and 600 °C, weak exothermic effects may be noticed which can be assigned to some oxidative degradation processes of the precursor resin. These oxidative degradation processes rely on the existing oxygen in the resin composition.

It has to be noted that the sample mass remaining after the water removal from the solution subjected to the thermal analysis was very small and therefore, the processes that took place over 400 °C were insufficiently

Sample no.	Reactants				Molar ratio
	Ca(NO <sub>3</sub> ) <sub>2</sub>	Al(NO <sub>3</sub> ) <sub>3</sub>	Citric acid	Ethylene glycol	3:2:15:16.5
2	Ca(NO <sub>3</sub> ) <sub>2</sub>	Al(NO <sub>3</sub> ) <sub>3</sub>	Citric acid	-	3:2:15
3	CaCl <sub>2</sub>	AlCl <sub>3</sub>	Citric acid	Ethylene glycol	3:2:15:16.5
4	CaCO <sub>3</sub>	Al(OH)(CH <sub>3</sub> COO) <sub>2</sub>	Citric acid	Ethylene glycol	3:2:15:16.5





Fig. 1 TG and DTA curves of the mixture of raw materials corresponding to sample 1, recorded in nitrogen atmosphere

emphasized. To get more information regarding the processes development at higher temperatures, the sample was pre-fired at 400  $^{\circ}$ C for 1 h and only afterwards subjected to thermal analysis.

Figure 2 shows the TG and DTA curves of the precursor 1, pre-fired at 400  $^{\circ}$ C/1 h, recorded in nitrogen atmosphere.

As result of pre-firing the sample at 400  $^{\circ}$ C, in the range 20–500  $^{\circ}$ C, TG curve shows a low and continue mass loss associated with some resin residues decomposition and accompanied on the DTA curve by a small but large endothermic effect.

The strong endothermic effect at 808.6 °C accompanied by a significant mass loss was associated with the decomposition of CaCO<sub>3</sub> resulted from the polymeric resin degradation. The large endothermic effect between 950–1100 °C, accompanied by mass loss on TG curve, could be assigned to the unoxidative degradation of the last organic residues from the resin.

The results of the FTIR analysis shown below evidence the presence of organic residue in the samples annealed at 600 and 850  $^{\circ}$ C.

The behaviour of the polymeric resin 1, pre-fired at 400 °C, subjected to thermal analysis in air atmosphere (Fig. 3) essentially differ in the range 350–650 °C compared with its behaviour in nitrogen atmosphere.

In this case, the DTA curve (Fig. 3) shows a large exothermic effect between 400 and 580 °C, accompanied



Fig. 2 TG and DTA curves of the precursor 1, pre-fired at 400 °C/ 1 h, recorded in nitrogen atmosphere



Fig. 3 TG and DTA curves of the precursor 1, pre-fired at 400  $^{\circ}$ C/ 1 h, recorded in air atmosphere

by mass loss on TG curve. This effect is due to the combustion reactions of the organic residues resulted from the resin degradation, reactions favoured by the presence of the oxygen in the working atmosphere. The weak exothermic effect at 615.5 °C, accompanied also by mass loss, is associated with the burning of organic carbon left behind by the resin degradation. CaCO<sub>3</sub> decomposition is in this case also pointed out on the DTA curve at 821.5 °C, accompanied by mass loss. In the 850–1200 °C range, the sample behaviour is similar, whether the working atmosphere was nitrogen or air. The endothermic effect above 850 °C is pointed out in both nitrogen and air atmosphere. The endothermic effect which appears in nitrogen atmosphere between 930 and 1100 °C can be also observed in air atmosphere but, in this case, the endothermic effect and the mass loss are smaller.

The thermal analysis in air atmosphere of samples 2-4, pre-fired at 400 °C are shown in Figs. 4, 5, 6.

From the comparative analysis of the four samples thermal behaviour, the following conclusions result: all the samples present on the DTA curve, the endothermic effect associated with the CaCO<sub>3</sub> decomposition to CaO and CO<sub>2</sub> (at 821.5 °C—sample 1, 807.6 °C—sample 2, 822.5 °C—sample 3 and 844.8 °C—sample 4); therefore, regardless the used calcium salt (nitrate, chloride, carbonate), the C<sub>3</sub>A obtaining is preceded by the CaO formation. Relatively low decomposition temperature of CaCO<sub>3</sub>, around 820 °C,



Fig. 4 TG and DTA curves of the precursor 2, pre-fired at 400  $^{\circ}C/$  1 h, recorded in air atmosphere



Fig. 5 TG and DTA curves of the precursor 3, pre-fired at 400  $^\circ\text{C}/$  1 h, recorded in air atmosphere



Fig. 6 TG and DTA curves of the precursor 4, pre-fired at 400  $^{\circ}$ C/ 1 h, recorded in air atmosphere

suggests that the resulted CaO is present in a fine dispersed and highly reactive form.

The CaCO<sub>3</sub> presence in the samples annealed at 600  $^{\circ}$ C is supported by the XRD results (Fig. 7).

In all the samples annealed at 600 °C, the single crystalline phase present is  $CaCO_3$  (calcite). The explanation for the presence of this phase is the reaction between the CaO and CO<sub>2</sub> (resulted from the resin degradation) forming CaCO<sub>3</sub>. The decomposition of CaCO<sub>3</sub> at temperatures below 850 °C is also supported by RX diffraction analysis—that shows the lack of CaCO<sub>3</sub> (calcite) at this temperature for all the samples (Fig. 8).



Fig. 7 XRD patterns of samples 1, 2, 3, and 4 annealed at 600 °C/1 h



Fig. 8 XRD patterns of samples 1, 2, 3 and 4 annealed at 850 °C/1 h

In the temperature range 350–650 °C, the behaviour of samples 1 and 4 is similar. Sample 2, differing from sample 1 only by the lack of ethylene glycol, shows two distinct exothermic effects between 350 and 650 °C, unlike sample 1 presents a single large exothermic effect. This behaviour could be explained by the fact that the ethylene glycol present in sample 1 participates at polycondensation processes with the carboxyl groups by the citric acid excessively used, resulting a resin in which the Ca<sup>2+</sup> and Al<sup>3+</sup> cations distribution is statistical.

Unlike samples 1, 2 and 4, which present strong exothermic effects between 350 and 650 °C, sample 3 presents only a weak exothermic effect between 420 and 550 °C with a small mass loss. This behaviour can be explained by the fact that, the resin degradation during the sample prefiring at 400 °C was more advanced for sample 3 (starting from chlorides) compared with samples 1, 2 and 4.

The weak exothermic processes between 850 and 930 °C for samples 1, 2 and 4 are associated with the reaction between the newly formed CaO and the  $Al_2O_3$  present in the mixture, forming  $C_{12}A_7$  and after that, the reaction between  $C_{12}A_7$  and CaO, resulting  $C_3A$ . These effects lack in the case of sample 3.

Over 930 °C, the DTA curves of samples 2 and 4 point out weak exothermic effects with a small mass loss, similar to sample 1.

Assigning these effects to the unoxidative resin degradation is supported by the observation made on samples removed from the platinum crucible: even after reaching the temperature of 1000 °C samples were grey at the bottom, whilst the colour at the top was pure white. The presence and the possible influence of the highly dispersed residual carbon on the C<sub>3</sub>A formation should not be neglected. This residual carbon could prevent the Al<sub>2</sub>O<sub>3</sub> crystallization process during the temperature rise, keeping it into a reactive form which enters in reaction with the very reactive CaO resulted from the CaCO<sub>3</sub> decomposition. This assumption is supported by the existing observations in literature, according to which, the excess of citric acid favours the formation of C<sub>3</sub>A [29].

Unfortunately, the XRD analysis do not reveals the presence of a crystallized aluminium precursor for any of the samples. For this reason, one can only make suppositions based on the thermal analysis results regarding the aluminium precursor that reacts with CaO forming  $C_3A$ .

The results of the phase analysis for the samples annealed at 850 °C show differences depending on the source of  $Ca^{2+}$  and  $Al^{3+}$  cations. In samples 1 and 2 (where nitrates of calcium and aluminium were used) and also in sample 4 (where calcium carbonate and basic aluminium acetate were used), C<sub>3</sub>A is already present alongside C<sub>12</sub>A<sub>7</sub> and CaO. In sample 3, at 850 °C was revealed only C<sub>12</sub>A<sub>7</sub> and CaO whilst C<sub>3</sub>A is absent.

At 1050 °C, the XRD analysis (Fig. 9) shows the presence of a single-phase  $C_3A$  only in the samples 1, 2 and 4. As the phase composition of sample 3 annealed at 600 °C proves the presence of CaCO<sub>3</sub> as in the case of the other samples, and the thermal analysis (Fig. 5) shows its decomposition at 822.5 °C, results that, the difference in case of sample 3 is the precursor for the Al<sup>3+</sup> cations. At 1050 °C, the phase analysis of sample 3 does not change compared to the phase analysis at 850 °C, what means that C<sub>3</sub>A was not formed.

Taking into account that a large part of diffraction maximum of  $C_{12}A_7$ ,  $C_3A$  and CaO overlap, the clear delimitation of these phases was made based on the following peaks at:  $2\theta = 18.126^{\circ}$  (only for  $C_{12}A_7$ ),  $2\theta = 47.626^{\circ}$  and  $2\theta = 59.272^{\circ}$  (only for  $C_3A$ ),  $2\theta = 53.856^{\circ}$  (only for CaO). The FTIR spectra of the samples 1–4 annealed at 600,

850 and 1050 °C are shown in Figs. 10, 11, 12, 13.

The results of the FTIR spectra are in accordance with the statements made on the bases of the thermal analysis and XRD spectra.

At 600 °C, all the samples present the specific bands of CO<sub>3</sub><sup>2-</sup> ions from CaCO<sub>3</sub>: 712, 880–860,1450–1410,1795 cm<sup>-1</sup> [30, 31]. The broad band located at 3450–3500 cm<sup>-1</sup> is due to –OH stretching vibration (intermolecular hydrogen bond) of the organic residue



Fig. 9 XRD patterns of samples 1, 2, 3 and 4 annealed at 1050 °C/1 h



Fig. 10 FTIR spectra of sample 1, annealed at 600, 850 and 1050 °C/1 h

[31]. The two bands located in the region  $2850-2927 \text{ cm}^{-1}$  are assigned to the asymmetrical and symmetrical stretching vibrations of CH<sub>2</sub> [31].

At 850 °C, in all samples spectra, the intensity of characteristic bands of CO<sub>3</sub><sup>2-</sup> ions decreases; the two bands located in the region 2850–2927 cm<sup>-1</sup> are present; instead of a broad band located at 3450–3500 cm<sup>-1</sup>, a sharp band appears, located at 3643 cm<sup>-1</sup> and assigned to free (monomeric) –OH [31]. The specific bands of calcium aluminates appear in the region 500–909 cm<sup>-1</sup>.



Fig. 11 FTIR spectra of sample 2, annealed at 600, 850 and 1050 °C/1 h



Fig. 12 FTIR spectra of sample 3, annealed at 600, 850 and 1050 °C/1 h



Fig. 13 FTIR spectra of sample 4, annealed at 600, 850 and 1050 °C/1 h

- At 1050 °C, all the samples show the characteristic bands of calcium aluminates. Between samples 1, 2 and 4 on one side and sample 3 on other side, there is a major difference, in full agreement with the XRD spectra: samples 1, 2 and 4 show the characteristic bands for  $C_3A$  [32], whilst sample 3 shows the characteristic bands for  $C_{12}A_7$ . The sharp band located at 1382.96 cm<sup>-1</sup> may be assigned to -OH group, resulted by the interaction of  $C_{12}A_7$  or CaO with atmospheric moisture.

For samples 1, 2 and 4, annealed at 1050 °C, containing single-phase  $C_3A$ , the specific surface area was performed. The obtained values were: 4.34 m<sup>2</sup> g<sup>-1</sup> for sample 1, 3.69 m<sup>2</sup> g<sup>-1</sup> for sample 2 and 3.31 m<sup>2</sup> g<sup>-1</sup> for sample 4. These values are comparable with those reported by Gülgün et al. [13] (4.2 m<sup>2</sup> g<sup>-1</sup>) at the C<sub>3</sub>A preparation starting from low polymerization degree PVA.

The larger specific surface area of sample 1 compared with sample 2 may be explained by the ethylene glycol presence in the precursor resin and the higher gas volume resulted in the resin degradation process. Comparing the specific surface area of samples 1 and 4, it can be noticed that the specific surface area of C<sub>3</sub>A depends also by the salt used as the source of the two cations. The smaller specific surface area of sample 4 suggests the starting of the C<sub>3</sub>A formation at a lower temperature than for sample 1 and at the temperature rise up to 1050 °C, a more advanced crystallization process takes place in sample 4.

#### Conclusions

The results of thermal analysis corroborated with the XRD investigations provided valuable information regarding the underlying processes for the  $C_3A$  synthesis using the polymeric precursor method. It was proved that  $CaCO_3$  (calcite) is the intermediate compound formed by the resin degradation in all the studied cases.

The synthesis of C<sub>3</sub>A as single-phase using the polymeric precursor method was conditioned by the raw materials used. C<sub>3</sub>A resulted as single-phase after annealing at 1050 °C for 1 h only starting from calcium nitrate or carbonate and aluminium nitrate or acetate as salts precursor for Ca<sup>2+</sup> and Al<sup>3+</sup> cations. The obtaining of C<sub>3</sub>A is preceded by the formation of C<sub>12</sub>A<sub>7</sub> and CaO, which leads to C<sub>3</sub>A according to the reaction:

$$C_{12}A_7 + 9 CaO = 7C_3A_7$$

Even if, using calcium and aluminium chlorides, the homogeneity of the  $Ca^{2+}$  and  $Al^{3+}$  cations in the precursor resin was performed at ionic scale,  $C_3A$  was not obtained. In this case, at 1050 °C, the only present phases were

 $C_{12}A_7$  and CaO. This shows that the two phases formed in the presence of chlorides have a lower reactivity.

The lack of ethylene glycol in the reaction mixture did not affect the C<sub>3</sub>A formation. This shows that –COOH and –OH, by the citric acid used in excess, lead to the formation of a resin, in a proportion which ensures the formation of C<sub>3</sub>A at 1050 °C.

Acknowledgements This study was partially supported by the strategic grant POSDRU/88/1.5/S/50783, Project ID50783 (2009), co-financed by the European Social Fund—Investing in People, within the Sector Operational Programme Human Resources Development 2007–2013.

## References

- 1. Gao X, Lei L, Lv C, Sun Y, Zheng H, Cui Y. Preparation and photoluminescence property of a loose powder,  $Ca_3Al_2O_6:Eu^{3+}$  by calcination of a layered double hydroxide precursor. J Solid State Chem. 2008;181:1776–81.
- Oh SH, Finones R, Jin S, Choi SY, Kim KN. Influence of tricalcium aluminate phase on in vitro biocompatibility and bioactivity of calcium aluminate bone cement. J Mater Res. 2004;19: 1062–7.
- Yang S, Kondo JN, Hayashi K, Hirano M, Domen K, Hosono H. Partial oxidation of methane to syngas over promoted C<sub>12</sub>A<sub>7</sub>. Appl Catal A. 2004;277:239–46.
- Ghoroi C, Suresh AK. Solid–Solid reaction kinetics: formation of tricalcium aluminate. AIChE J. 2004;53:2399–410.
- Mohamed BM, Sharp JH. Kinetics and mechanism of formation of tricalcium aluminate, Ca<sub>3</sub>Al<sub>2</sub>O<sub>6</sub>. Thermochim Acta. 2002;388: 105–14.
- Singh VK, Ali MM, Mandel UK. Formation kinetics of calcium aluminates. J Am Ceram Soc. 1990;73:872–6.
- Stephan D, Wilhelm P. Synthesis of pure cementitious phases by sol-gel process as precursor. Z Anorg Allg Chem. 2004;630: 1477–83.
- Douy A, Gervais M. Crystallization of amorphous precursors in the calcia–alumina system: a differential scanning calorimetry study. J Am Ceram Soc. 2000;83:70–6.
- Lazău I, Păcurariu C, Becherescu D, Sim A. The use of some unconventional methods in the calcium aluminates synthesis. Rom J Mater. 2001;3:203–9.
- Pati RK, Panda B, Pramanik P. Preparation of nanocrystalline calcium aluminate powders. J Mater Synth Process. 2002;10: 157–61.
- Lee SJ, Benson EA, Kriven WM. Preparation of Portland cement components by poly(vinyl alcohol) solution polymerization. J Am Ceram Soc. 1999;82:2049–55.
- Lee SJ, Lee CH, Kriven WM. Synthesis of oxide ceramic powders by polymerized organic inorganic complex route. J Ceram Process Res. 2000;1:92–5.
- Gülgün MA, Kriven WM, Nguyen H. Processes for preparing mixed metal oxide powders.US Patent No. 6 482 387 B1, 19 Nov 2002.
- Kingsley JJ, Suresh K, Patil KC. Combustion synthesis of fineparticle metal aluminates. J Mater Sci. 1990;25:1305–12.
- Fumo DA, Morelli MR, Segadaes AM. Combustion synthesis of calcium aluminates. Mater Res Bull. 1996;31:1243–55.
- Taş AC. Chemical preparation of the binary compounds in the calcia–alumina system by self-propagating combustion synthesis. J Am Ceram Soc. 1998;81:2853–63.

- Ianoş R, Lazău I, Păcurariu C, Barvinschi P. Peculiarities of CaO·6Al<sub>2</sub>O<sub>3</sub> formation by using low-temperature combustion synthesis. Eur J Inorg Chem. 2008;2008(6):925–30.
- Ianoş R. An efficient solution for single-step synthesis of 4CaO·Al<sub>2</sub>O<sub>3</sub>·Fe<sub>2</sub>O<sub>3</sub> powders. J Mater Res. 2009;24:245–52.
- Ianoş R, Lazău I, Păcurariu C, Barvinschi P. Fuel mixture approach for solution combustion synthesis of Ca<sub>3</sub>Al<sub>2</sub>O<sub>6</sub> powders. Cem Concr Res. 2009;39:566–72.
- Taş AC, Majewski PJ, Aldinger F. Chemical preparation of pure strontium-and/or magnesium-doped lanthanum gallate powders. J Am Ceram Soc. 2000;83:2954–60.
- Xu Y, Yuan X, Huang G, Long H. Polymeric precursor synthesis of Ba<sub>2</sub>Ti<sub>9</sub>O<sub>20</sub>. Mater Chem Phys. 2005;90:333–8.
- Bernardi MIB, Feitosa CAC, Paskocimas CA, Longo E, Paiva-Santos CO. Development of metal oxide nanoparticles by soft chemical method. Ceram Int. 2009;35:463–6.
- Oliveira HHS, Cebim MA, Da Silva AA, Davolos MR. Structural and optical properties of GdAlO<sub>3</sub>:RE<sup>3+</sup> (RE = Eu or Tb) prepared by the Pechini method for application as X-ray phosphors. J Alloy Compd. 2009;488:619–23.
- 24. Lazarevic ZZ, Vijatovic M, Dohcevic-Mitrovic Z, Romcevic NZ, Romcevic MJ, Paunovic N, Stojanovic BD. The characterization

of the barium titanate ceramic powders prepared by the Pechini type reaction route and mechanically assisted synthesis. J Eur Ceram Soc. 2010;30:623–8.

- 25. Pechini M. Method for preparing lead and alkaline earth titanates and niobates and coating method using the same to form a capacitor. US Patent No. 3,330,697, 11 July 1967.
- Gaki A, Chrysafi R, Perraki Th, Kakali G. Synthesis of calcium aluminates trough the polymeric precursors route. Chem Ind Chem Eng Q. 2006;12:137–40.
- Gaki A, Chrysafi R, Perraki Th, Kakali G. Chemical synthesis of hydraulic aluminate compounds using the Pechini technique. J Eur Ceram Soc. 2007;27:1781–4.
- Yuan X, Xu Y, He Y. Synthesis of CaAl<sub>4</sub>O<sub>7</sub> via citric acid precursor. J Alloy Compd. 2007;441:251–4.
- Yuan X, Xu Y, He Y. Synthesis of Ca<sub>3</sub>Al<sub>2</sub>O<sub>6</sub> via citric acid precursor. Mater Sci Eng A. 2007;447:142–5.
- 30. Moenke H. Mineralspektren. Berlin: Akademie-Verlag; 1962.
- Nakanishi K, Solomon PH. Infrared absorption spectroscopy. San Francisco: Holden-Day, Inc.; 1977.
- Ramachandran VS, Beaudoin JJ. Handbook of analytical techniques in concrete science and technology. Principles, techniques and applications. New York: William Andrew Publishing; 2001.